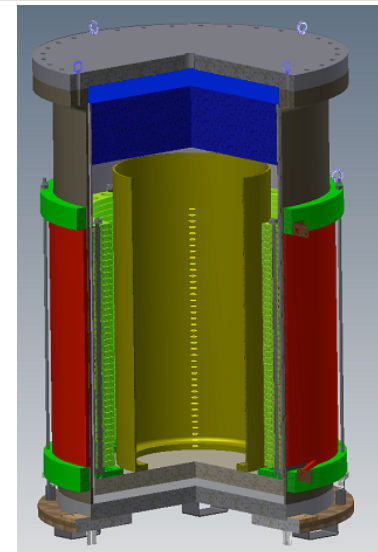
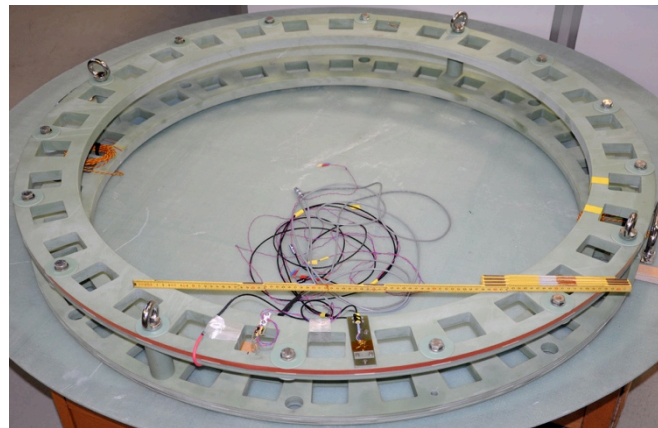
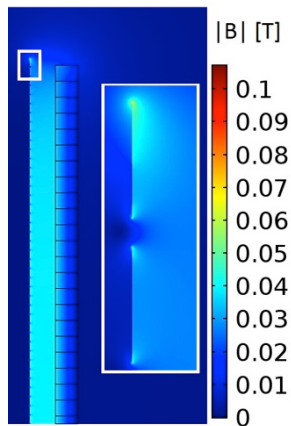


# SmartCoil –Shielded Core Reactor for Current Limitation on the Distribution Level

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18.09.2017, EUCAS 2017

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# Project profile

## Short description

- Design, construction und presentation of a novel nonlinear reactor coil for the fault current limiting (10 kV / 600 A single-phase)
- The concept uses a stack of superconducting shielding rings to reduce the impedance of the reactor during normal operation



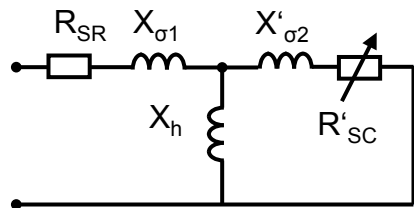
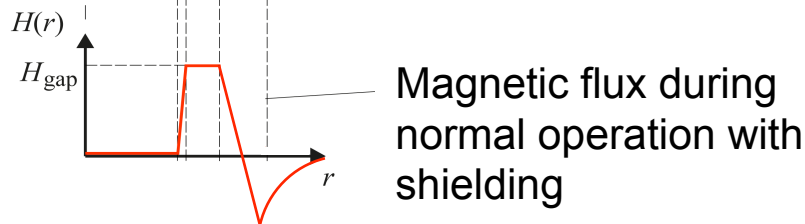
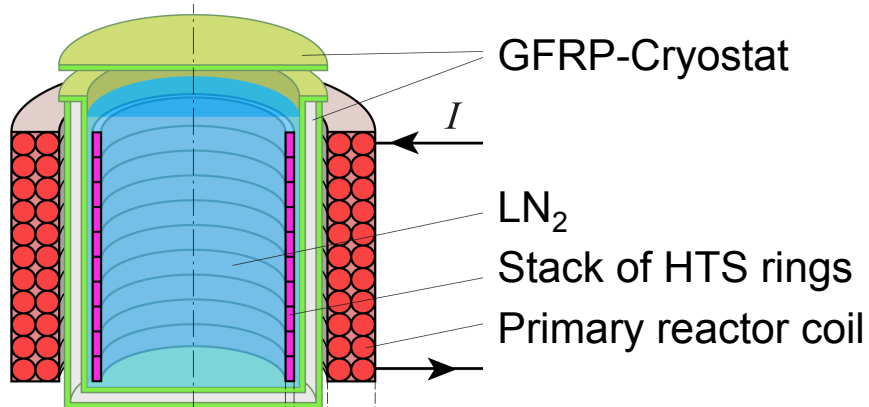
## Profile

- Project period: 09/2014 – 02/2018
- Funding: German Government, Federal Ministry for Economic Affairs and Energy (Grant 03ET7525A)
- Project partners:
  - Karlsruhe Institute for Technology (KIT)
  - Siemens AG



**SIEMENS**

# Project concept and specification



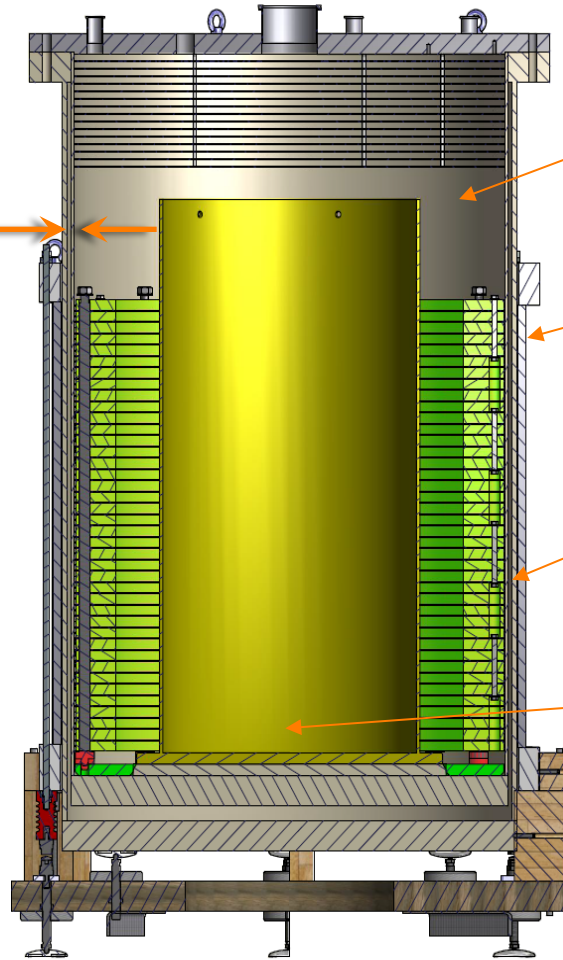
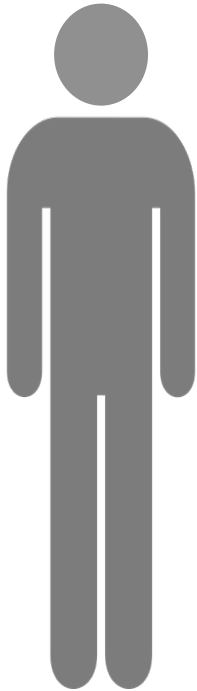
Gap must be narrow to decrease the stray impedance  $X_{\sigma 1}$ ,  $X'_{\sigma 2}$

## ■ Specification of SmartCoil (single-phase)

Protected power $S_{SFCL}$	3,46 MVA
Voltage $U_{SFCL}$ (10 kV / $\sqrt{3}$ )	5,774 kV
Rated current $I_D$	600 A
Frequency $f_n$	50 Hz
Fault limiting time $T_{lim}$	$\leq 100$ ms
Impedance of reactor coil	6%
<b>Impedance ratio between the limiting- and the nominal operation</b>	<b><math>\geq 4</math></b>

# Basic component parts of SmartCoil

Gap must be narrow to decrease the stray impedance  $X_{\sigma 1}$ ,  $X'_{\sigma 2}$



GFRP cryostat

Reactor coil (inductor)

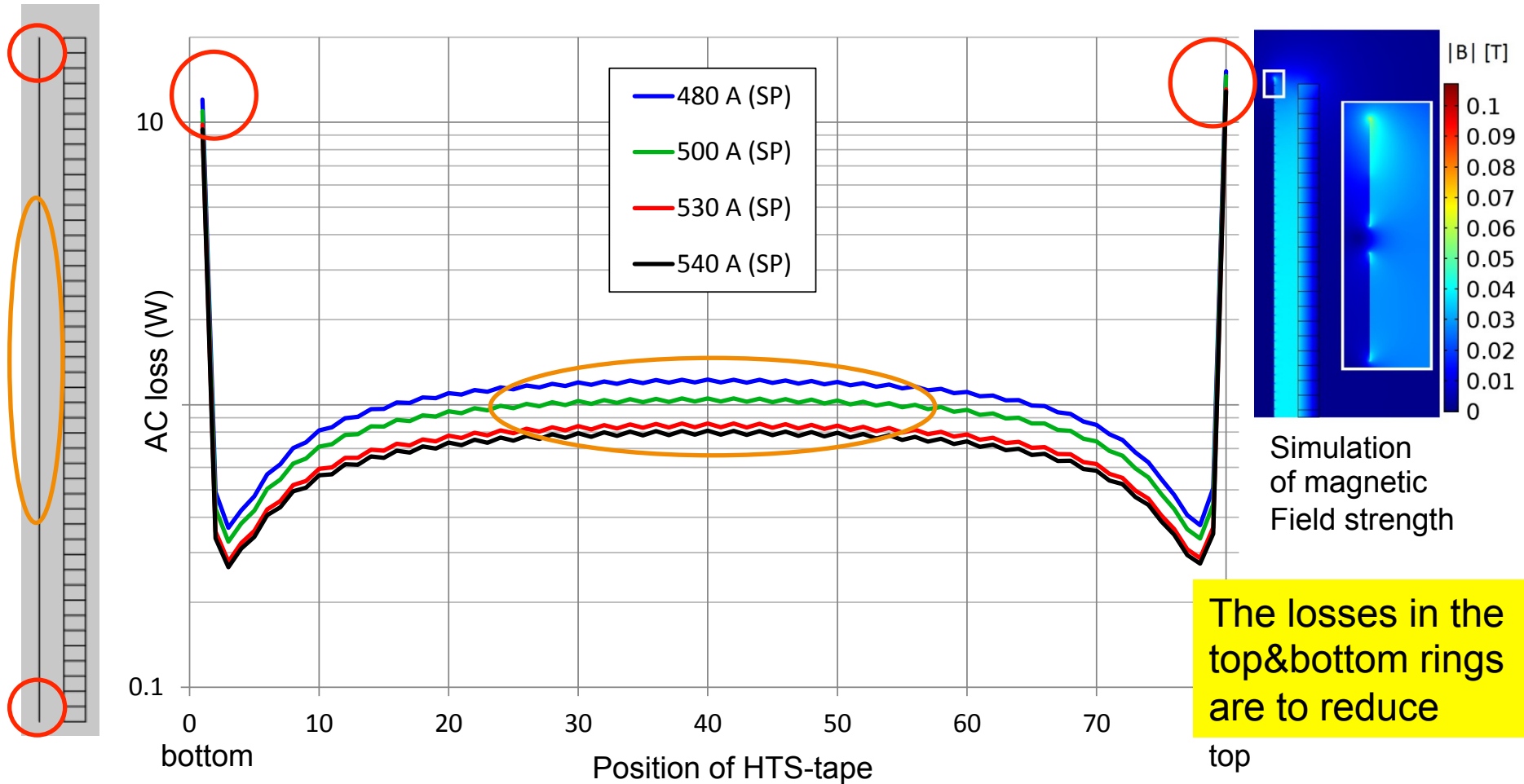
Superconducting inset:  
40 modules  
each with two HTS-rings

displacement body

assembly and transport platform

# Simulation of AC-losses in HTS nominal operation

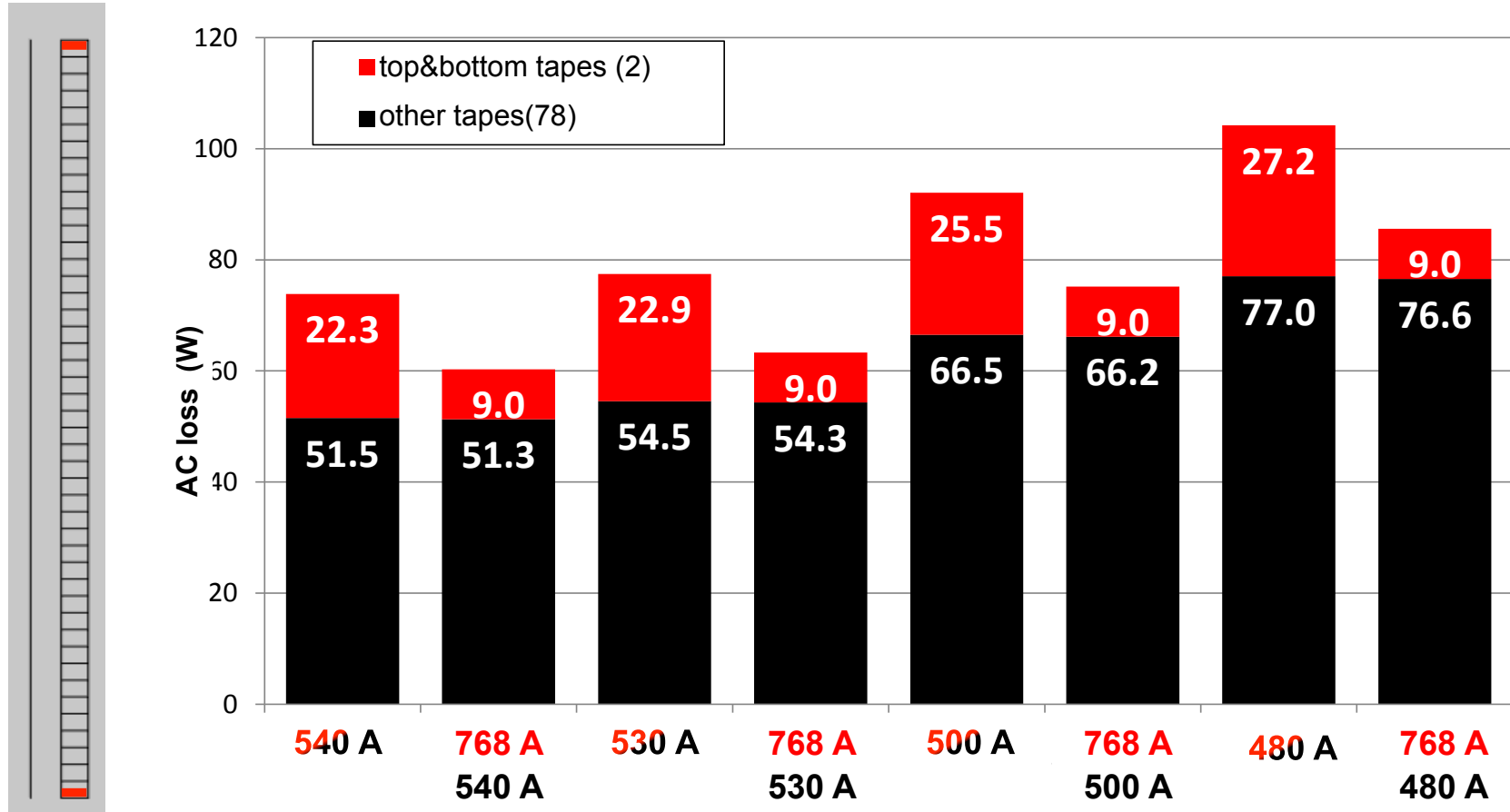
- Contribution of the individual HTS-rings to the AC-losses



The losses in the top&bottom rings are to reduce

# Simulated AC-losses in HTS rings nominal operation

- Contribution of the **top&bottom** rings to the AC-losses



HTS with the higher critical current will be used in the top&bottom rings

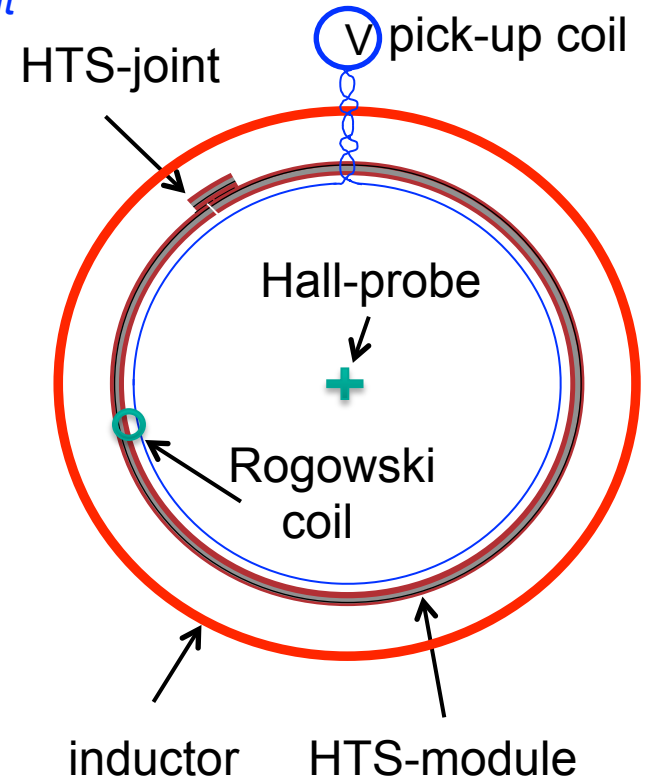
# Set-up for component test

## ■ DC-test

- Measurement of critical current  $I_C$
- Measurement of contact resistance  $R_{joint}$
- Conform to specification?
- Any degradation in test?

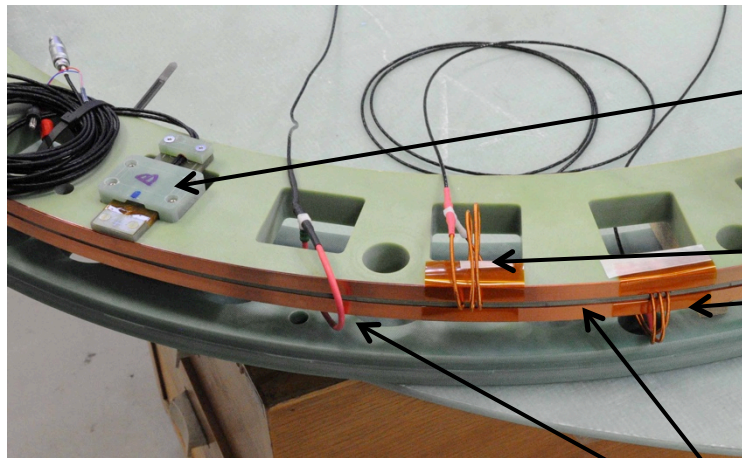
## ■ AC-test

- Quench of HTS
- Imitation of the fault conditions
- Thermal cycles



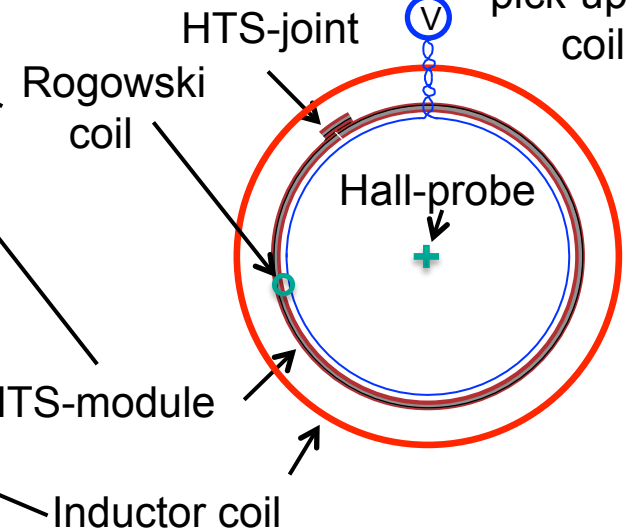
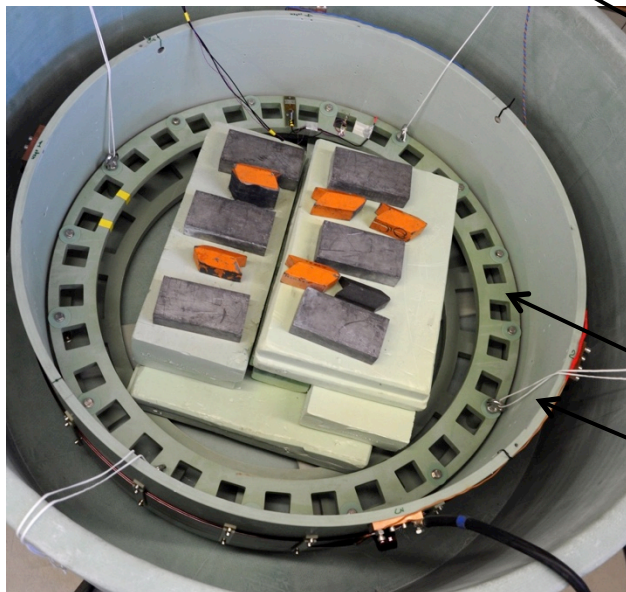
contactless measurement on HTS-ring

# Set-up for component test: DC/AC



Hall probe on the HTS module

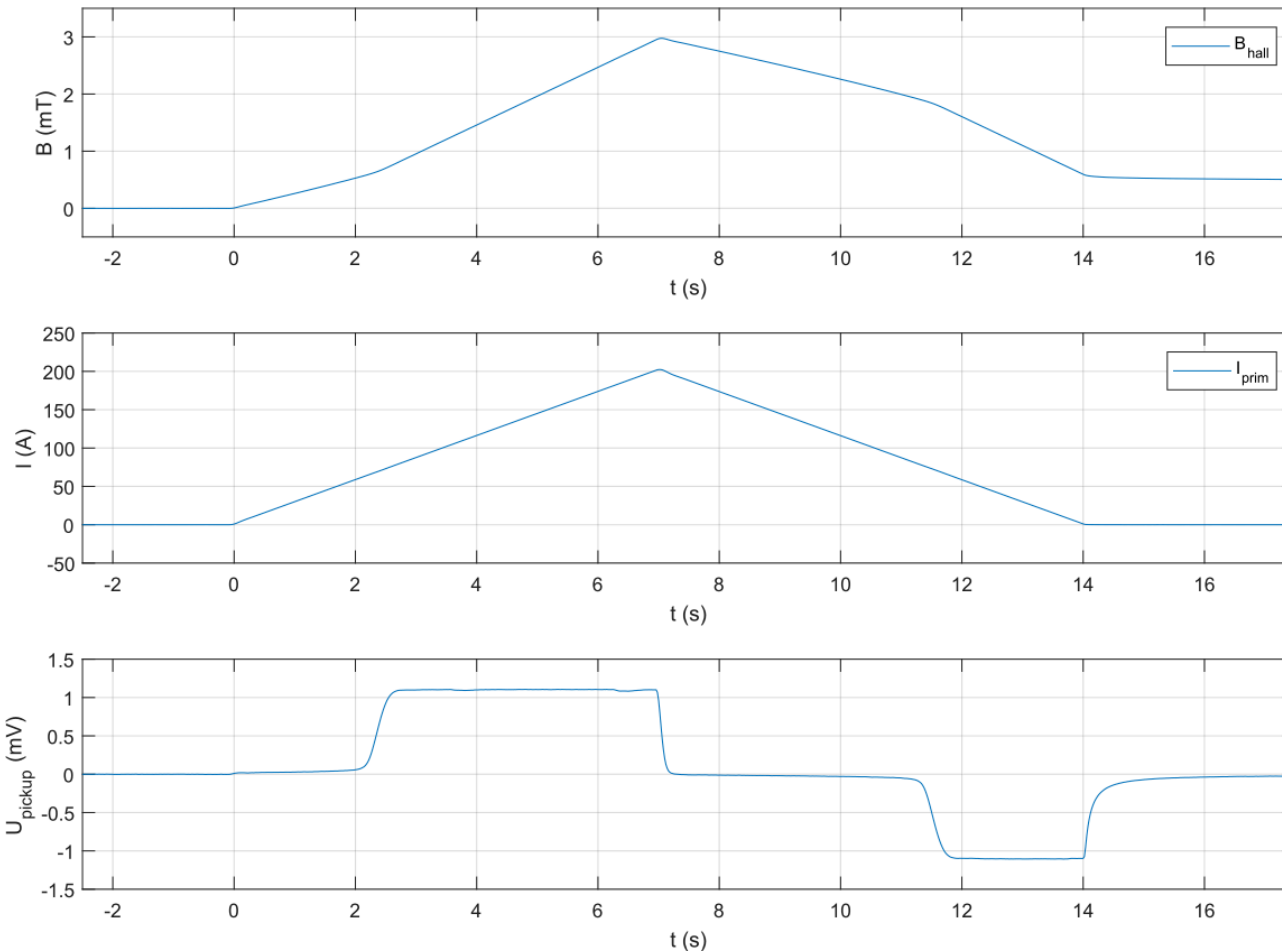
Rogowski coils for each tape  
upper HTS-ring  
lower HTS-ring





# DC-testing of HTS-module (1 HTS ring)

## Determination of $I_C$ using the inductor and pick-up coils

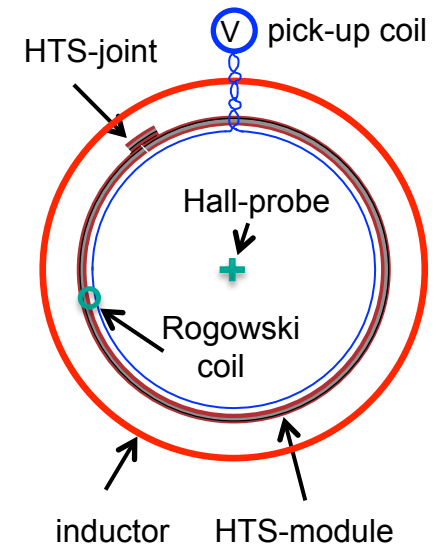


### measure:

$B_{\text{hall}}$ : central magnetic field

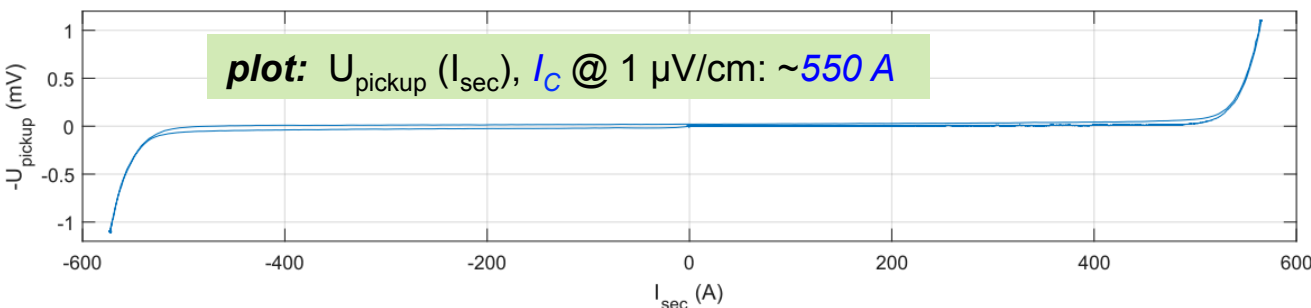
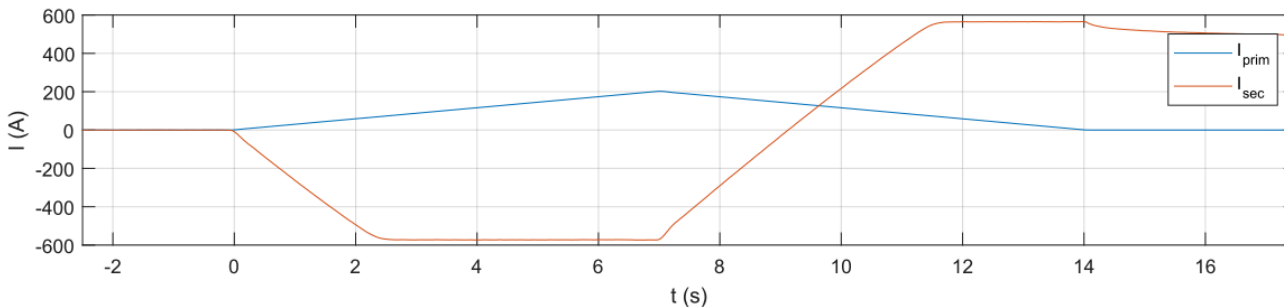
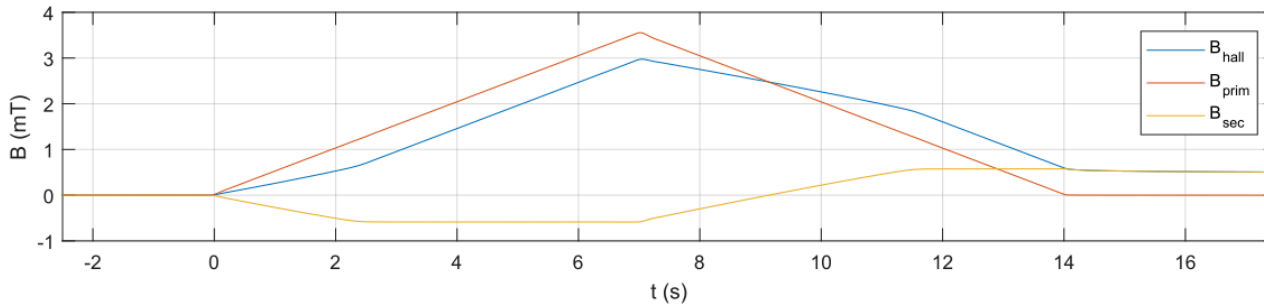
$I_{\text{prim}}$ : primary current

$U_{\text{pickup}}$ : pickup voltage



# DC-testing of HTS-module (1 HTS ring)

## Determination of $I_C$ using the inductor and pick-up coils

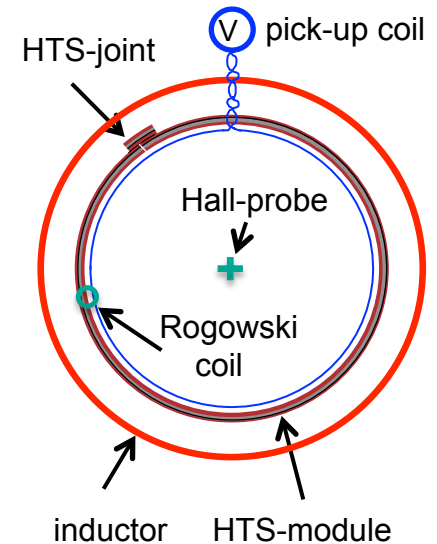


**calculate:**

$$B_{\text{prim}} = 17.56 \times 10^{-6} \text{ T/A} * I_{\text{prim}}$$

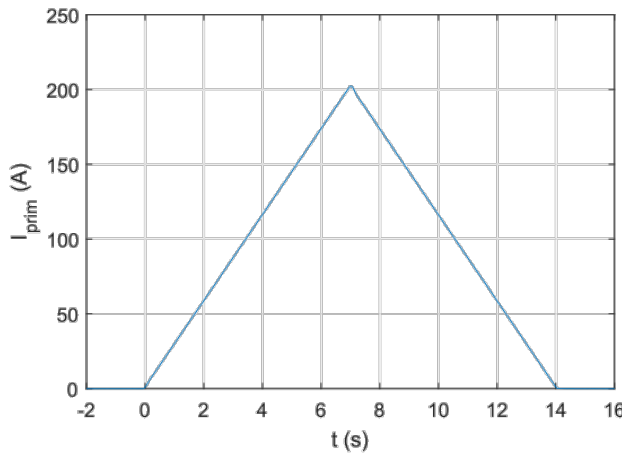
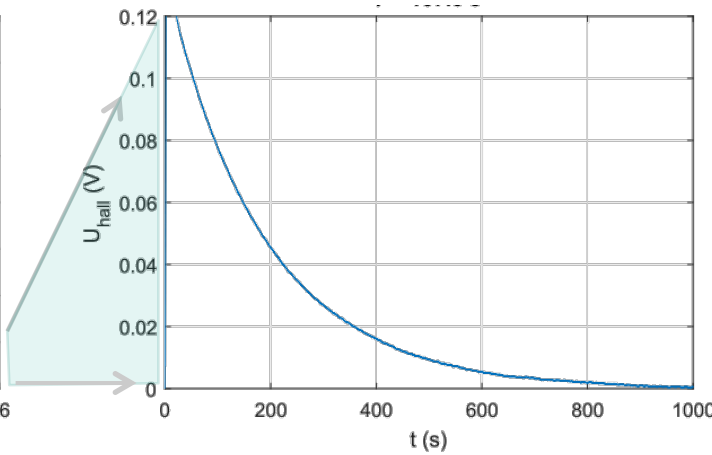
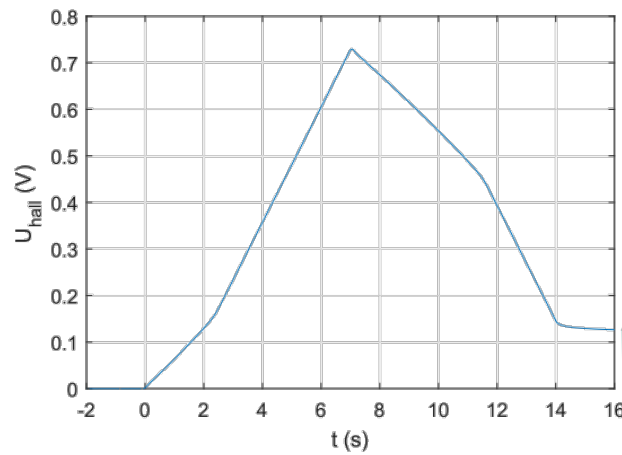
$$B_{\text{sec}} = B_{\text{hall}} - B_{\text{prim}}$$

$$I_{\text{sec}} = 0.9807 \times 10^6 \text{ A/T} * B_{\text{sec}}$$



# DC-testing of HTS-module (1 HTS ring)

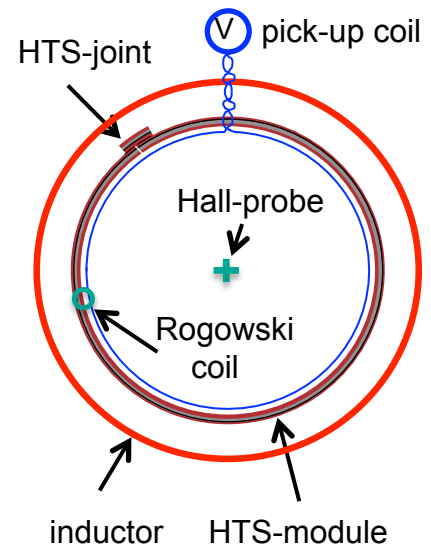
## Determination of $R_{joint}$ using the inductor and the Hall-probe



exponential decay of  $U_{hall}$   
after  $I_{prim}$  is back to zero:

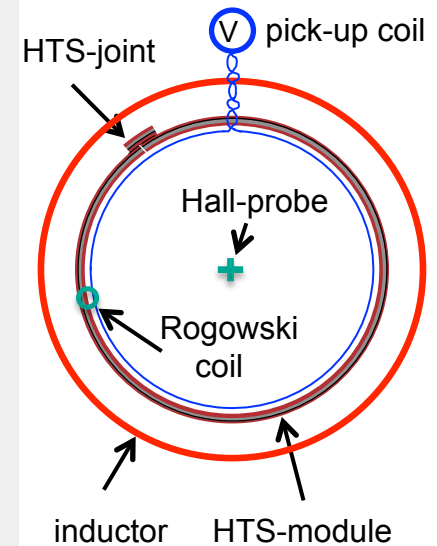
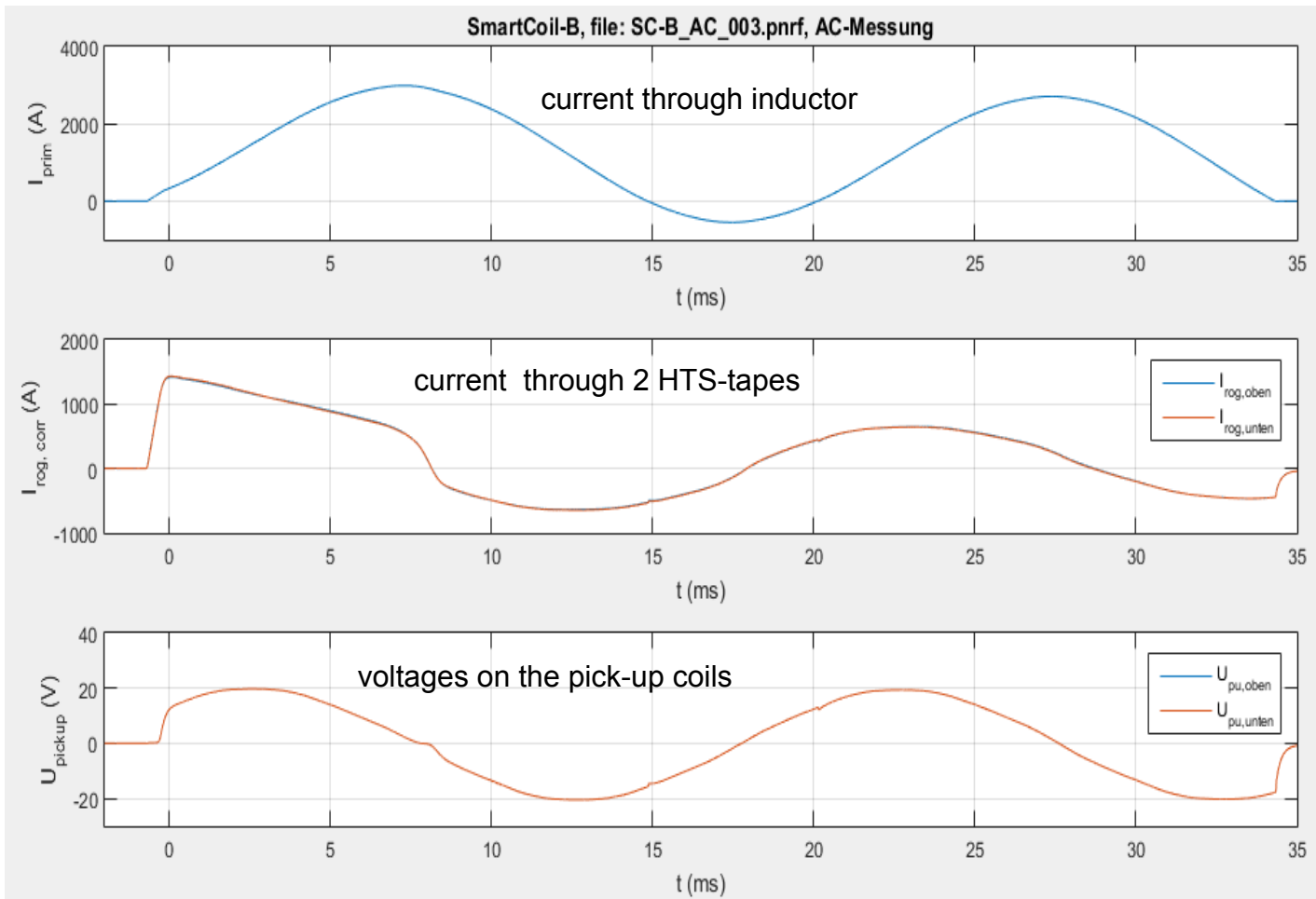
$$\tau = 188 \text{ s,}$$

$$R_{joint} = L / \tau = 4.21 \text{ } \mu\text{H} / 188 \text{ s} = 22 \text{ n}\Omega$$



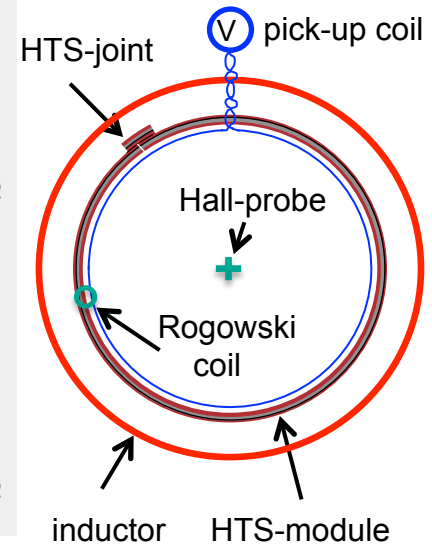
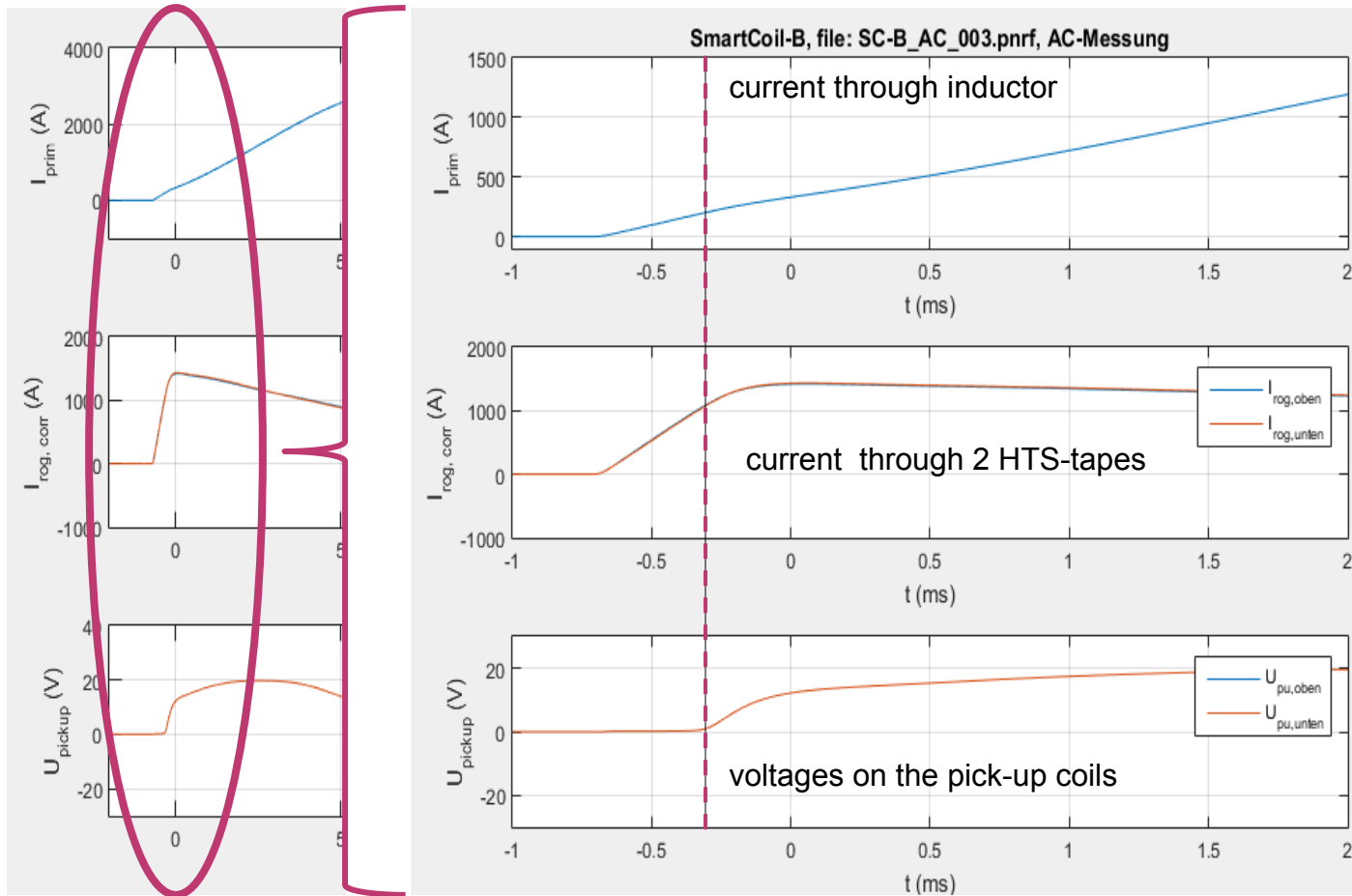
# AC-testing of HTS-module

## ■ Quenching transients



# AC-testing of modul

## ■ Quenching transients - zoom in, the time-axis expanded



## ■ Completed work steps and achieved results

- Design of the fault current limiter (single-phase 3,46 MVA)
- Specification, choice and qualification of 2G HTS
- Simulations of 2G HTS to optimize the geometry and the losses
- Specification of the GFRP cryostat with particularly small wall thickness
- Developing of suitable contacting method for HTS rings (soldering)
- In-situ determination of critical current and contact resistance
- 26 (of 40 needed) HTS modules are manufactured and tested

## ■ Next steps

- Delivery of the GFRP cryostat
- Production and tests of remaining HTS components
- Installation and performance tests of the entire system in the field
  - Determination of losses in rated operation mode
  - Demonstration of the limiting capacity

# Many thanks to the project team and to the companies involved in SmartCoil

## Project (core) team

Anne Bauer (Siemens)  
Jörg Brand (Ingenieurbuero Brand)  
Otto Batz (Siemens)  
Steffen Elschner (KIT, HS Mannheim)  
Michael Frank (Siemens)  
Wilfried Goldacker (KIT)  
Hans-Peter Krämer (Siemens)  
Andrej Kudymow (KIT)  
Oliver Näckel (KIT)  
Marijn Oomen (Siemens)  
Christian Schacherer (Siemens)  
Severin Strauss (KIT)  
Peter van Haßelt (Siemens)  
Johann Willms (Synergie)  
Viktor Zermeno (KIT)

## Companies involved

AMSC  
Fabrum Solutions  
ILK Dresden (GRP Cryostat)  
STI  
SuNAM  
SuperOx  
SuperPower  
THEVA  
Trench Austria

# Add-on reactor coil

Specification of inductor	
Rated current	600 A
Rated voltage (Leiter-Erde)	5.77 kV
Height of inductor	1170 mm
Inner diameter	1318 mm
Number of turns	45
Number of layers	1
Nominal impedance	1.95 mH (0.60 $\Omega$ )
Short-circuit voltage	6 % ( -> 1.2 % )
Operating temperature	< 155 °C

