# How material selection and processing affect the final magnetic properties

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### JC and his Bs&T...



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   make and design forrite 2Cx and 2Ex
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marketing nanocrystalline VP500F components



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- Introduction
- Ferrite material review 1990 2020
- Material selection and processing
- Final properties
- Summary

### **Sinus Magnetization AC**



**Pulse Magnetization** 



## Critical review of ferrite material development of last decades

- 1995 2005
   classic way: loss density@100°C reduction due to improvement of iron oxide purity

   FXC: 3C8x ->3C9x, 3C91/90/93
   TSC: TSF 8040,7070,5099
   TDK: PC30->PC40, 46/45/44->47
   engineering crystalline anisotropy to ensure *thermal* design convergence @ 100°C
   T.C.<0</li>
- 2005 2015
   temperature dependence of loss density is "disappeared"
   **7.C.=0 95er** phenomen: ALLFLAT, PC95/N95/3C95
   engineering to have two zero K<sub>1</sub> vs. T with Co<sup>2+</sup> on the octahedral site
- 2015 dito diversification of *95er* material A/F, W/H... and Positive temperature coefficient for mateiral over MHz PC200/210/220

T.C. temperature coefficient\* under large excitation

T.C.>0

#### 95er effect: MAGNETOCRYSTALLINE ANISOTROPY-COBALT

Optimum Cobalt

+

 $K_1$ 

Co<sup>2+</sup>

In MnZn-Ferrites Co<sup>2+</sup> is generally accepted to be located on the octahedral B-sites In addition Co<sup>2+</sup> because of its electronic structure and its interaction with the crystal magnetic field has a strong positive contribution to the anisotropy.

Co<sup>2+</sup>

More than Optimum Cobalt

### H.F. Material competition landscape

- Pronounced magnetocrystalline anisotropy (loss level overall due to high purity Fe<sub>2</sub>O<sub>3</sub>) 3C80->3C90->3C94->3C97 PC30->PC40->PC44->PC47 N 27->N 67->N 87->N 97
- Dopants and microstructure

*ferrite is artificial ceramic, a semiconductor (new kids on the block) A. Goldman 90')* powdering processing (chemical and mechanical nature); compacting and sintering (powder metalllurgical nature); (air)gapping, lapping (surface engineering nature); potting and conditioning of terminals, assemblying (mechanical engineering nature) clearly, application is *just* another postprocessing of ferrite making

• Competition: ferromagnetic material from alloy -> with higher B<sub>s</sub> and higher T<sub>c</sub>

nanocrystalline tape wound core to substitute toroidal ferrite \* metal alloyed powdered shaped core to challenge gapped ferrite design, mostly from thermal point of view \*\*

\* Further reading: damp oscillation of nanocrystalline tape woud core for common mode choke \*\* Further reading: damp oscillation of metal alloyed powdered core

## Loss volume density vs. Temperature comparison @ 100 kHz 200 mT



## Loss volume density vs. T behavior in MHz range, size matters !



The ferrite loss increasing with high operation temperature, like copper The core size, not only the material, is important for high frequency application

kHz 10'

5 10<sup>2</sup>

101

5 10<sup>3</sup>

### **Design relevant parameters of inductive component**

• Transformer design

for high frequency efficient energy conversion, the only uncertainty is loss ! simple treatement with Steinmetz coefficient (only 3 parameters), otherwise at least further 3 parameters needed to describe the loss vs. temperature dependence **95er** phenomen pleased circuit designer research of loss is unfortunately reduced to "renaissance" of Steinmetz with data puzzle

• Choke design

a dc biased high frequency ripple design can always to be approached with gapped ferrite core, the thermal management is of experimental nature, the thermal resistance\* is simplified to describe typical behavior The current validation of magnetic components, only for PCB components standard IEC 62024 Ed.2 for rated current < 22 A

• Discrepency between typical and limit value increases

\* Further reading: Hanna Curve reloaded with BsT-pulse

### **Further processing 1 Disaccomodation**



Picture 1: undisturbed disaccomodation  $\frac{\Delta \mu_e}{\mu_e} = d_e lg \frac{t_E}{t_A}$ Picutre 2: complete disturbed discaccomodation with reference  $\mu_B$ (2 h after full impetus)

Picture 3: disturbed disaccomodation with reference  $\mu_B$ (2 min each partial impetus),  $\eta$  as impetus ratio Picture 4: relationship  $\eta$  vs. ratio of  $H_{AC}/H_c H_{AC}$  as impulsed fieldstrength, and  $H_c$  as coecivity,  $\eta$  can be generalized as thermodynamic and mechanical impetus

G. Roespel **1968** 

### **Further processing 2 dynamic load**



frequency f of shaking stress

in centrifuge

#### **Further processing 3 static axial load**



Hysterese loop of *perminvar* NiZnFerrite under different axial pressure



### **Energy expression and its magnitude (soft magnetics)**

Energy terms	Coefficient	Definition	Range
Exchange energy	A (J/m)	Material constant	10 <sup>-12</sup> – 2·10 <sup>-11</sup> J/m
Anisotropy energies	K <sub>u</sub> , K <sub>c</sub> (J/m <sup>3</sup> )	Material constant	± (10 <sup>-1</sup> – 10 <sup>4</sup> ) J/m <sup>3</sup>
<i>External</i> field energy	H <sub>ex</sub> J <sub>s</sub> (J/m <sup>3</sup> )	<i>H<sub>ex</sub></i> = <i>external field</i> J <sub>s</sub> = saturation magnetization	Open, depending on <b>field</b> magnitude
Stray field energy	K <sub>d</sub> (J/m³)	$K_{d} = J_{s}^{2}/2 \mu$	$0 - 3.10^{6} \text{ J/m}^{3}$
External stress energy	$\sigma_{ex}\lambda$ (J/m³)	$\sigma_{ex}$ = external stress $\lambda$ = magnetostriction constant	Open, depending on <i>stress</i> magnitude
Magnetostrictive self energy	$C\lambda^2$ (J/m <sup>3</sup> )	C = shear modulus	$0 - 10^3 \text{ J/m}^3$

It is impossible to assign a single origin for domain structures in all kinds of materials. The non-local energy terms, stray field energy, are responsible for the development of domains, i.e. loss

The thermodynamically stabile domain treatment of uniform, reversible magnetiaztion is material characterisation The considerable different magnitude of anisotropies in shape and size delivers more argument for core characterisation

### Major technological bottleneck: validation technique

- Loss mechanism still not understood, no analytic micromagnetic model (defects, disclosure etc.), loss measurement, like domain analysis, is indispensible material loss – core loss – power loss – energy loss
- Standard confusion & ignorance TC68 alloy vs. TC51 ferrite

the major difference in loss measurement of alloy and ferrite, is the systemic influence of temperature dependence.

material / core / component

material characteristic: core characteristic: closed magnetic circuit open magnetic circuit



- Vertical integration of ferrite making as business consequence TDK, material – core – component – system.....
- Much easier to communicate about good & bad results, rather than about magnetics (material TC68/core IEEE393/coil IEEE389)
- The existing IEC standards helpful to understand ferrite, IEC62044-2 for small signal and IEC62044-3 for large signal
- Soft ferrite is right in midlife-crisis,
  - 80 years after discovery, meticulous research in magnetism in 40-50s (Snoek, Néel) extensive material research in 70-80s (International Conference Ferrite) experienced flourish business with SMPS (MOSFET) in 90-00s facing now challgenge by other new kids (rapid quenched alloys) 10-20s can be helped with better understanding by application engineers for WBG applications